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**PATENT APPLICATION FOR
A TUNABLE MICROWAVE MULTIPLEXER**

BY

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A TUNABLE MICROWAVE MULTIPLEXER

FIELD OF THE INVENTION

5 The invention is related to the field of tunable multiplexers. More particularly, this invention relates to a tunable multiplexer which can effectively couple ceramic or metallic resonator filters with TEM resonator filters. The multiplexer provides contiguous channel spacing and wide resonant frequency band tuning.

10 BACKGROUND OF THE INVENTION

 Multiplexers are used to combine a plurality of channels, each centered at a different frequency, into one combined signal. The same multiplexer can be used to separate a single signal carrying many frequencies or channels into the constituent
15 channels, each channel located at its respective frequency.

 In the prior art, multiplexers have been designed by connecting bandpass filters in parallel or series to combine the plurality of channels. Relatively simple decoupling techniques work to separate the constituent channels provided that the channels are
20 separated by frequency spacings equivalent to several passbands of the individual filters. However, when the channels of the multiplexer are too close in frequency, the interaction of the nearby channels will significantly degrade the performance of the multiplexer. Simple decoupling techniques prove ineffective at frequencies this close.

25 When the channels of the multiplexer are contiguous, the multiplexer should be designed as an integral unit. One method of achieving this is disclosed in the paper "A Technique for the Design of a Multiplexer Having Contiguous Channels¹," hereby incorporated by reference. The channel filters are connected in parallel using high

¹ G.L. Matthaei and L. Young, "A Technique for the Design of Multiplexer Having Contiguous Channels," IEEE Trans. Microwave Theory Tech., vol. MTT-12, pp. 88-93, Jan. 1964.

impedance coupling wire. In addition, a susceptance-annulling network using a low-impedance line added at the common port results in a nearly constant total input admittance. However, it is very difficult to design and manufacture the coupling wires needed to achieve the required couplings and low imaginary impedance over all channels or frequency bands at the common port.

The paper "A Generalized Multiplexer Theory²," hereby incorporated by reference, discloses the use of a common transformer to produce planar structure duplexers, star shaped combline filters and interdigital multiplexers. However, this method is limited to use with TEM resonator structures.

U.S. Patent No. 5,262,742, hereby incorporated by reference, discloses a half wavelength transmission line used as a common resonator or common transformer. The common resonator is used to couple two combline filters to a common antenna port. However, like the method disclosed in "A Generalized Multiplexer Theory," this method is limited to use with TEM resonator structures.

SUMMARY OF THE INVENTION

Referring now to the figures, in which like numerals refer to like elements, the present invention is shown. The invention comprises a tunable microwave multiplexer. Within the multiplexer is a plurality of channel filters comprising at least one resonator for filtering microwave and RF signals. The channel filters are coupled to a combining/dividing mechanism. The combining/dividing mechanism comprises a common port and a common resonator coupled to the common port.

In another embodiment, the invention comprises a microwave communication system comprising a receiver for receiving RF and microwave signals, a transmitter for transmitting RF and microwave signals, a signal processor coupled to the receiver and transmitter for processing signals and at least one antenna coupled to the receiver and the

² J.D. Rhodes and R. Levy, IEEE Trans. Microwave Theory Tech., vol. MTT-27, pp. 111-123, Feb. 1979.

transmitter. Either the receiver or the transmitter can comprise a tunable microwave multiplexer. The tunable microwave multiplexer comprises a plurality of channel filters comprising at least one resonator for filtering RF and microwave signals. In addition, the multiplexer contains a combining/dividing mechanism coupled to the plurality of channel
5 filters via coupling apertures. The combining/dividing mechanism comprises a common port and a multiple half-wavelength coaxial resonator coupled to the common port. In addition, the tunable microwave multiplexer contains transmission ports coupled to the plurality of filters.

10 In still another embodiment, the invention comprises a method of multiplexing a plurality of microwave channel frequencies. This method includes the steps of inputting a signal comprising a plurality of frequency channels into a common resonator. In addition, the phase difference between a common port of a common resonator to each RF
15 port of a plurality of cavity channel filters is maintained at approximately 0 or 180 degrees. Furthermore, the signal comprising a plurality of frequency channels is separated into its constituent frequency signals. Still furthermore, at least one of said plurality of frequency channels is output.

BRIEF DESCRIPTION OF THE DRAWINGS

20 Fig. 1 is a configuration of a 4-channel tunable multiplexer, according to one embodiment of the present invention.

Fig. 2 is a configuration of a common resonator, according to one embodiment of the
25 present invention.

Fig. 3 is a measured frequency response of a 4-channel tunable multiplexer, according to one embodiment of the present invention.

30 Fig. 4 is drawing of the tunable multiplexer housing, according to one embodiment of the present invention.

Fig. 5 is a circuit diagram of a 4-channel tunable multiplexer using a common resonator, according to one embodiment of the present invention.

5 DETAILED DESCRIPTION OF ONE EMBODIMENT OF THE INVENTION

Referring now to the figures, in which like numerals refer to like elements, the present invention is shown. The present invention consists of a tunable microwave multiplexer 1 comprising a plurality of channel filters 2-8 coupled to a
10 combining/dividing mechanism. In a preferred embodiment, the plurality of channel filters 2-8 can be either dielectric loaded resonators or combline resonators, while the combining/dividing mechanism is preferably a common resonator 20.

The tunable microwave multiplexer 1 can be used in a microwave communication
15 system that both receives and transmits RF and microwave signals. The tunable microwave multiplexer can be used to both multiplex and demultiplex RF and microwave signals. An example of a microwave communication system that can be used is found in Patent No. 4,578,815, hereby incorporated by reference.

20 The tunable multiplexer 1 operates in the following manner. A signal comprising a plurality of microwave signal frequencies is input at a common port 10. The signal will pass through the common resonator 20. A signal frequency from one of the plurality of microwave signals will couple into a filter 2-8 if the passband of the filter is tuned to the frequency of the microwave signal. On the other hand, if the passband of the filter is
25 tuned to a different frequency, then the filter 2-8 will reject the microwave signal. In this manner, the plurality of microwave signals will be separated.

The tunable multiplexer 1 can also be used to combine signals of different frequencies. Signals of different frequencies are input via transmission ports to a channel
30 filter 2-8 that will pass its respective frequency. The signals will be combined into one

signal comprising these different signal frequencies in the common resonator 20. The composite signal is then output through the common port 20.

Multiplexer

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The tunable microwave multiplexer 1 has a common port 10 into which a signal comprising a plurality of microwave signal frequencies is input. In a preferred embodiment, the common port 10 can be a single coaxial cable connector (see Fig. 1). The common port 10 can be coupled to the common resonator 20 using a tapped-in or
10 loop configuration.

Use of a common resonator combining/dividing structure for the multiplexer 1 can maintain the phase difference of the RF signal from the common port 10 of the common resonator 20 to each RF port of the cavity channel filters 2-8 at precisely 0 or
15 180 degrees. Thus, there is no phase difference or displacement where the channel filters 2-8 interface with the common resonator 20. Therefore, no critical phasing transmission line is needed in the multiplexer 1. As a result, microwave channel frequencies can be combined or divided efficiently over a broad bandwidth.

Half-Wavelength Coaxial Resonator

In a preferred embodiment, the common resonator is a multiple half-wavelength coaxial resonator 20 (see Fig. 1). The coaxial resonator's length is a multiple half-wavelength of the average frequency of the multiplexer 1. Stated another way, the
25 physical length of the coaxial resonator 20 is a multiple half-wavelength of the average frequency of the input signal comprising a plurality of microwave signal frequencies input at common port 10. Therefore, the coaxial resonator 20 appears as a low impedance to any of the input channel frequencies.

30 The coaxial resonator 20 is operated at a higher order TEM mode. Thus, either the magnetic field or the electric current is a maximum at both ends of the resonator 20.

In addition, there is a quarter wavelength difference in phase between the electric and the magnetic fields. Consequently, when the magnetic field is a minimum, the electric field is a maximum and vica-versa.

5 An adjustment screw SC1 (accessible from the outside of the enclosure of the coaxial resonator 20) is used to adjust the resonant frequency of the coaxial resonator 20 (see Fig. 2). It is positioned where the electric field is a maximum in the coaxial resonator 20. By changing the resonant frequency of the coaxial resonator 20, a new center frequency is selected.

10 In a preferred embodiment, the coaxial resonator 20 comprises an enclosure E1, a cavity 28 and an inner conductor C1 (see Fig. 2). The inner conductor C1 is either milled into the resonator cavity 28 or affixed into the cavity 28 using the same conductive material as that used for the resonator's 20 enclosure E1. This ensures that the
15 conductive material maintains good contact over temperature.

Both the magnetic and the electric fields vary periodically every half-wavelength along the half-wavelength coaxial resonator 20. Thus, there are multiple maximum magnetic field positions distributed along the resonator 20. Coupling apertures 60, 62, 64
20 and 66 (see Fig. 1 and Fig. 2) located on the enclosure wall EW1 of the common resonator 20, are positioned at the peaks of the magnetic field respectively. The signal input to the common port 10 is radiated through these coupling apertures 60-66. In a preferred embodiment, four channel filters 2, 4, 6 and 8 (see Fig. 1) are coupled to the coupling apertures 60 through 66 of the coaxial resonator 20 respectively. This allows
25 for efficient coupling of the channel filters to the common port 10 of the multiplexer/demultiplexer 1 and optimized compactness of the housing.

Channel Filters

30 In a preferred embodiment, the plurality of channel filters 2-8 can consist of either dielectric loaded resonators or combline resonators. In a preferred embodiment, the

dielectric loaded resonators can be made from a ceramic material. In another preferred embodiment, the combline resonators can be made from a ceramic material. In still another preferred embodiment, the combline resonators can be metallic resonators.

5 Fig. 1 discloses a preferred embodiment of the tunable microwave multiplexer/demultiplexer 1 that contains four filters 2, 4, 6 and 8, connected in parallel. In a preferred embodiment, each channel filter comprises two resonators, 32, 34, 36, 38, 40, 42, 44 and 46 (for a total of eight resonators) which are located in two cavities, 12, 14, 16, 18, 20, 22, 24 and 26 (for a total of eight cavities), respectively. For example, 10 filter 2 comprises resonators 32 and 34 located in cavities 12 and 14 respectively. The two resonators 32 and 34 are connected in series.

 The individual resonators 32-46 may be regarded as filter sections. An increase in the number of resonators 32-46 (or filter sections) connected in series produces a steeper skirt on the passband of the respective filter 2-8 which results in sharper attenuation of 15 undesired frequencies. It should be noted that while four filters 2-8 containing two resonators 32-46 are shown, any number and combination of filters and resonators may also be used in accordance with what the specification discloses. Fig. 3 is an exemplary plot of the measured frequency response of a 4-channel tunable multiplexer 1.

20 The cavities 12-26 are located within a housing 3 (see Fig. 1 and Fig. 4). In a preferred embodiment, the housing 3 is made from a conductive material such as aluminum, although other metals will also work well. In addition, a common enclosure wall 5 separates the cavities 12 through 26. Fig. 1 shows that the two resonators 32-46 of 25 each channel filter, 2, 4, 6 and 8, are coupled together by apertures 50, 52, 54 and 56 respectively, opened on the common enclosure wall 5 between the two resonators.

 In a preferred embodiment, the dielectric resonator used is disclosed in copending U.S. patent application 60/155,600, Tunable, Temperature Stable Dielectric Loaded 30 Cavity Resonator and Filter, hereby incorporated by reference. In a preferred

embodiment, the filters are tunable. A tuning element assembly can be used to adjust the frequency.

As stated above, the amount of coupling between the channel filters 2-8 and the common port 10 of the multiplexer 1 is controlled by the size and the location of the coupling apertures, 60 through 66. Energy from the multiple half-wavelength coaxial resonator 20 is coupled through the coupling apertures 60 through 66 and into the filters (2, 4, 6 and 8 respectively) via the filter resonator 32-44 connected to that aperture 60-66, respectively. The other end of each filter not connected to the coupling apertures is connected to a transmission port. Transmission ports TX1 through TX4 are connected to filters 2, 4, 6 and 8 respectively (see Fig. 1). In a preferred embodiment, transmission ports TX1 through TX4 can each be a single coaxial cable connector (see Fig. 1). Each transmission port TX1-TX4 can be used to output one of the channel frequencies separated by the tunable multiplexer 1. In addition, it can be used as an input to receive a single channel frequency which will be combined in coaxial resonator 20 with other received channel frequencies from other transmission ports TX1-TX4 and output through common port 10.

Circuit Diagram

Fig. 5 is a circuit diagram of a 4-channel tunable multiplexer 1, according to one embodiment of the present invention. Electrical circuit 100 illustrates schematically the circuit formed by the half-wavelength common resonator 20 and four channel filters 2-8 of Fig. 1. Transformer M_{com} represents common port 10. Transformers M01₁ through M01₄ represent the coupling apertures 60 – 66 located on the enclosure walls E1 of the common resonator 20. Transformers M12₁ through M12₄ represent apertures 50 – 56 opened on the common enclosure wall between the two resonators through which the two resonators of each channel filter 2-8 are coupled together, respectively. Transformers M23₁ to M23₄ represent transmitting ports TX1 through TX4, respectively.

